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Abstract

This paper aims to clarify the optimum amount of fumed silica (SiO_2) nanofiller in resisting the initiation and propagation of electrical treeing in silicone rubber (SiR). Unlike other works, SiR/SiO_2 nanocomposites containing seven different weight percentages of SiO_2 nanofiller were prepared for this purpose. To achieve the objective, the electrical tree characteristics of the SiR/SiO_2 nanocomposites were investigated by comparing the tree initiation voltage, tree breakdown time, tree propagation length and tree growth rate with its equivalent unfilled SiR. Moreover, the structural and morphological analyses were conducted on the SiR/SiO_2 nanocomposite samples. The results showed that the SiR, when added with an appropriate amount of SiO_2 nanofiller, could result in an improved electrical tree resistance. It implies that the 5 wt% of silica is the optimum amount to achieve the optimal electrical tree resistance such that above 5 wt%, the tree resistance performance has been abruptly reduced, subjected to the agglomeration issue.

Keywords: electrical treeing, nanocomposites, silica, silicone rubber

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1. Introduction

Polymeric insulating materials have become an important part of high voltage apparatuses over two decades [1, 2]. The main function of polymeric insulating materials in high voltage apparatuses is to provide electrical insulation. However, degradation processes occur in polymeric materials, which subsequently jeopardize the insulation performance of the materials. Such degradation processes are normally initiated by small electrical sparks, also popularly known as partial discharges [3].

In light of the foregoing, electrical treeing is one of the partial discharge phenomena that commonly results in the degradation of polymeric insulating materials [4]. Therefore, electrical tree resistance of polymeric insulating materials needs to be improved. This can be achieved by mixing two or more different types of polymers to form polymer blend materials [5-7]. Promising improvements of polymeric insulating materials against partial discharge activities were also reported when certain amounts of inorganic/organic nanofillers were mixed with polymers [8-10].

Recently, polymer nanocomposite insulating materials are gaining popular interests from dielectric researchers in attempts to improve polymers' resistance against electrical degradation processes with the addition of nanofillers [11-13]. In this regard, the improved resistance of nanocomposites against partial discharges is commonly attributed to the nanometer-sized nature of the fillers that contributes to the presence of large interfacial areas between the polymers and the nanofillers [14-16]. Consequently, the addition of nanofillers in polymers has led to in enhanced partial discharge resistance and electrical tree resistance of polymer nanocomposites [17]. Not only addition of nanofillers but the quantity of silica nanofiller influenced the initiation time of electrical treeing and the resistance towards electrical treeing in solid insulation [18-21].

In line with the development of nanocomposites in electrical insulation, researchers discovered that the performance of silicone rubber (SiR) could also be enhanced when

the material is added with nanofillers. SiR, a widely used polymeric material in industrial applications, has been used as a coating material for high voltage outdoor insulators especially for glasses and ceramics to help reducing maintenance costs and resist potential flashovers of the insulators [22-24]. Besides that, SiR has also been used as insulating materials for cable accessories such as to joint materials and stress cones [25, 26].

Since the use of SiR in high voltage insulation systems, many studies have been conducted to understand its role in improving insulation performance [27, 28]. However, the electrical properties, especially the electrical tree resistance of SiR, when added with SiO₂ nanoparticles, are less explored. Also, the optimum formulation of SiO₂ nanofillers that can effectively suppress the growth of electrical treeing in SiR has not been well studied and clarified. This article, therefore, reports on the characterization of the electrical tree characteristics of SiR based nanocomposites when added with a different weight ratio of SiO₂ nanoparticles. The optimal SiR/SiO₂ nanocomposite formulation towards electrical tree characteristics has been discussed accordingly.

2. Methodology

The sample preparation and experimental setup procedure are elucidated in this section.

2.1. Sample Preparation

Fumed or pyrogenic SiO₂ nanofiller, obtained from Sigma Aldrich, with a specific particle size of 12 nm, was used as a nanofiller. The Sylgard 184 SiR elastomer, obtained from Dow Corning, was used as a polymer. The SiR is of the Polydimethylsiloxane (PDMS) type and belongs to a group of polymeric organosilicone compounds referred to as silicones. It is optically clear, inert, non-toxic and non-flammable.

The mixing process of SiR and fumed SiO₂ nanofillers was performed with the aid of a magnetic stirrer. SiR and SiO₂ nanofillers were mixed at a speed of 125 rpm for 1 hour. Ultrasonicator (Fisher, FB705BX) was used in the mixing process to ensure that the SiO₂ nanoparticles were dispersed in SiR matrices. The dispersion energy, power operation, and amplitude were more than 100 kJ, between 100-150 W, and 70%, respectively.

A re-weighing process was carried out after the sonication process because some weight losses were expected during the redeployment process from one beaker to another at the mixing stage. After completing the re-weighing process, the SiR/SiO₂ nanocomposites were mixed with a hardener based on 10:1 SiR to hardener ratio, for 15 minutes at 125 rpm. The SiR/SiO₂ nanocomposites were further mixed using a magnetic stirrer. The next step was the degasification process to remove potential voids and bubbles formed in the SiR/SiO₂ nanocomposites during the mixing process. The degasification process was performed by using a vacuum oven for 25 minutes at 27 °C. Afterwards, the SiR/SiO₂ nanocomposite sample was cast onto the electrodes gap on a microscope slide glass. Then, the leaf-like specimen was covered with a microscope cover glass. The leaf-like specimen of SiR/SiO₂ nanocomposites was cured at 100 °C for 45 minutes inside a vacuum oven. Table 1 shows the compositions of SiR/SiO₂ nanocomposites prepared for electrical treeing tests.

laple	ble 1. Sample Compositions of SIR/SIO2 Nanocomposites	
	Sample Number	Nanocomposite Compositions
	1	Unfilled SiR
	2	SiR+1 wt% SiO ₂
	3	SiR+2 wt% SiO ₂
	4	SiR+3 wt% SiO ₂
	5	SiR+4 wt% SiO ₂
	6	SiR+5 wt% SiO ₂
	7	SiR+6 wt% SiO ₂
	8	SiR+7 wt% SiO ₂

Table 1. Sample Compositions of SiR/SiO2 Nanocomposites

2.2. Experimental Setup

Images of electrical treeing in unfilled SiR and SiR/SiO₂ nanocomposites were captured with the aid of an online monitoring system. The online monitoring system consisted of three main parts, i.e., a personal computer, a stereo microscope and a charge-coupled device (CCD) camera–the Olympus SZX16 Research Stereomicroscope equipped with an auxiliary DP-26

Olympus CCD camera was used. The camera has 72 times magnification capability and it was interfaced to a computer manufactured by Olympus Corporation. Each test specimen was placed in a container filled with silicone oil to avoid potential flashover during the experiment.

Figure 1 shows the experimental setup for the electrical treeing study. The needle electrode of each leaf-like specimen was connected to an AC high voltage source while the plane electrode was connected to the ground. A voltage source of 220 V with a frequency of 50 Hz was used as a supply to the voltage regulator. The voltage regulator regulated the HV transformer from 0 to 30 kV. The apparent power of the HV transformer was 1.38 kVA with a maximum output current of 14 mA. A 6100 Ω , 60 W high voltage resistor was connected in series with the secondary side of HV transformer and the needle electrode. The purpose of the HV resistor was to limit the current flow when a short circuit occurred. A high-resolution field emission electron microscope (FESEM) and a Fourier transform infrared (FTIR) spectroscope was later used to study the morphology of the samples.



Figure 1. The equivalent circuit of the experimental setup

3. Results and Discussion

Treeing analysis and chemical and physical bonding study were explained in detail in this section.

3.1. Treeing Analysis

The tree inception voltage, tree breakdown time, tree propagation length and tree growth rate of the investigated nanocomposite samples were analysed.

3.1.1. Tree Inception Voltage

The dependence of the tree inception voltage of SiR on nanofiller loading levels is shown in Figure 2. The tree inception voltage was higher for all SiR/SiO₂ nanocomposite samples compared with the unfilled SiR. The tree inception voltage for the unfilled SiR was 9.4 kV. The tree inception voltage increased with increasing nanofiller loading levels, with the highest voltage at 19.4 kV for SiR/SiO₂ nanocomposites containing 7 wt% of SiO₂.

3.1.2. Tree Breakdown Time

Figure 3 shows the tree breakdown time for unfilled SiR and SiR/SiO₂ nanocomposites with 1 wt%, 2 wt%, 3 wt%, 4 wt%, 5 wt%, 6 wt% and 7 wt% of SiO₂ nanofiller. The unfilled SiR recorded the earliest tree breakdown time compared with the SiR/SiO₂ nanocomposites. The tree breakdown time of the unfilled SiR was 151 s. For the SiR/SiO₂ nanocomposites, the tree breakdown time increased with increasing amounts of SiO₂ up to 5 wt%; the tree breakdown time for samples containing 1 wt%, 2 wt%, 3 wt%, 4 wt% and 5 wt% of SiO₂ loadings in SiR were 316 s, 621 s, 745 s, 1082 s and 1362 s, respectively. At 6 wt% and 7 wt% of SiO₂ loading levels, tree breakdown time reduced dramatically–the tree breakdown time is, however, longer than the unfilled SiR; the tree breakdown time for samples containing 6 wt% and 7 wt% SiO₂ became 234 s and 213 s respectively.



Figure 2. Tree inception voltage of SiR with different SiO2 loading levels



Figure 3. Tree breakdown time of SiR with different SiO2 loading levels

3.1.3. Tree Propagation Length

For the SiR/SiO₂ nanocomposites, the measurement of the electrical tree propagation length was done in the axial direction between the tip of the needle and the plane electrode. Based on Figure 4, the trees in nanocomposite samples with 1 wt%, 2 wt% and 3 wt% of SiO₂ bridged the gap of the needle and plane electrodes (2000 μ m) at 400 s, 700 s and 900 s, respectively. For samples containing 4 wt% and 5 wt% of SiO₂ nanofiller, the electrical trees did not bridge the gap of the needle and plane electrode – these samples recorded electrical tree propagation lengths of 1877 μ m and 1631 μ m, respectively, after the electrical trees propagated for 1000 s. Meanwhile, the electrical trees in the samples with 6 wt% and 7 wt% of SiO₂ propagated rapidly until breakdown occurred. It is noteworthy that these samples were chosen as representatives of the overall electrical tree propagation length for each sample type [1].



Figure 4. Tree propagation lengths of SiR with different SiO₂ loading levels

The growth rate of electrical treeing for unfilled SiR and SiR/SiO₂ nanocomposites with 1 wt%, 2 wt%, 3 wt%, 4 wt%, 5 wt%, 6wt% and 7 wt% of SiO₂ nanofiller loading levels is shown in Figure 5. The growth rate of electrical treeing in SiR with 0 wt%, 1 wt%, 2 wt%, 3 wt%, 4 wt%, 5 wt%, 6 wt% and 7 wt% were 11.99 μ m/s, 8.55 μ m/s, 4.57 μ m/s, 3.86 μ m/s, 3.25 μ m/s, 2.58 μ m/s, 68.66 μ m/s and 89.21 μ m/s, respectively.



Figure 5. The growth rate of electrical treeing of unfilled SiR and SiR/SiO₂ samples filled with different SiO₂ contents

3.1.5. Electrical Treeing Channel

The electrical tree channels for all investigated samples were analyzed based on the propagation of electrical trees upon the initiation of treeing. The electrical tree images for nanocomposite samples containing 1 wt%, 2 wt%, 3 wt%, 4 wt%, 5 wt%, 6 wt% and 7 wt% of SiO₂ and pure SiR are shown in Figures 6 (a-h), respectively. Of note, the electrical treeing for all nanocomposite samples were of the branch type.



(e) (f) (g) (h)

Figure 6. Electrical tree images for samples containing (a) pure SiR (b) 1 wt%, (c) 2 wt%, (d) 3 wt%, (e) 4 wt%, (f) 5 wt%, (g) 6 wt% and (h) 7 wt% of SiO₂; the measurement scale is 200 μ m

3.2. Chemical and Physical Bonding Study

The chemical and physical bondings were analysed using field emission scanning electron microscopy and Fourier transform infrared spectroscopy.

Clarification of the optimum silica nanofiller amount for electrical treeing resistance (Z. Nawawi)

3.2.1. Field Emission Scanning Electron Microscopy

The dispersion state of the SiO₂ nanofiller in SiR was analyzed using Field Emission Scanning Electron Microscopy (FESEM). Figures 7(a-e) show SEM micrographs for nanocomposite samples containing 1 wt%, 3 wt%, 5 wt%, 6 wt% and 7 wt% of SiO₂, respectively. SiO₂ nanofillers have larger specific surface areas than the conventional particulate filled system. SiO₂ nanofillers are closely located with their neighboring nanofillers. Due to the small size of nanoparticles, large interfacial areas exist between the SiO₂ nanofillers in the SiR, which is considered to be one of the key roles leading to the unique properties of nanocomposites. This interfacial area can be considered as an interaction zone or zan interphase. The interaction zone at the surface of SiO₂ nanofillers could cause the nanofillers to be attached physically in the SiR matrices. This attachment results in the structure of SiR becoming densely packed and robust. From the micrographs, fine-sized SiO₂ particles can be observed in all the nanocomposite samples. Agglomerated SiO₂ particles can also be observed in part of the samples. As the amount of SiO₂ increased to 6 wt% and 7 wt%, increased nanoparticle agglomerations can clearly be observed, as in Figures 7 (d) and 7 (e) for the nanocomposite samples containing 6 wt% and 7 wt% of SiO₂, respectively.



Figure 7. SEM micrographs of nanocomposite samples containing (a) 1 wt%, (b) 3 wt%, (c) 5 wt%, (d) 6 wt%, and (e) 7 wt% of SiO_2

3.2.2. Fourier Transform Infrared Spectroscopy

Figure 8 shows the Fourier Transform Infrared (FTIR) spectra for the SiO_2 nanofiller and the nanocomposite samples containing 0 wt%, 1 wt%, 3 wt%, 5 wt%, 6 wt% and 7 wt% of SiO_2 . The characteristic transmittance band of SiO_2 nanofiller can be observed at 1110 cm⁻¹. The spectrum corresponds to the silicone (Si-O) bonding.



Figure 8. FTIR spectra of SiO₂ powder and nanocomposite samples containing 1 wt%, 3 wt%, 5 wt%, 6 wt% and 7 wt% of SiO₂ and pure SiR

4. Discussion

The SEM micrographs showed that fine-sized SiO₂ particles could be observed in all the nanocomposite samples. Increasing the amount of SiO₂ nanofiller, however, resulted in increasing amounts of SiO₂ particle agglomerations. Meanwhile, the FTIR spectra indicated that the SiO₂ nanofiller had strong physical interactions with the SiR. The additional polymer chains that were inserted into the SiO₂ confined the polymer nanoscopically. The interaction between the SiO₂ and SiR resulted in the formation of a highly ordered structure due to the presence of neighbouring chains that surrounded mobile SiR chains. Hence, molecular orientation of the chains became higher, and further additional crosslinks in the system were formed [29].

From the electrical tree images, a densely packed electrical tree structure was observed when the amount of SiO₂ in SiR increased. The formation of the densely packed tree structure could cause the electrical trees to be difficult to initiate in the SiR matrices. Therefore, the tree inception voltages for all the SiR/SiO₂ nanocomposites were higher compared with the unfilled SiR.

In addition, SiO₂ nanofiller itself could also be the key factor contributing to the higher tree inception voltages and longer tree breakdown times of the SiR/SiO₂ nanocomposites (up to 5 wt% of SiO₂ loading levels) than the unfilled SiR. The presence of SiO₂ nanofiller could slow down the electrical tree propagation process since the nanofiller could serve as physical obstacles to curb the growth of the electrical treeing. In this regard, the electrical trees are expected to grow along the surface of the SiO₂ nanofiller.

Meanwhile, the presence of SiO₂ nanofiller in SiR could create trapping sites. SiO₂ nanofillers could trap charge carriers from the needle electrodes after the high voltage was applied. The trapped charge carriers required high energy to move from one trap to another trap. So, the electrical charge mobility was reduced due to the presence of the trapping sites. The reduction of electrical charge carrier mobility along the nanofiller and SiR interfaces could be a major factor in improving the dielectric properties and causing the growth of electrical treeing to become slower for the nanocomposite samples containing up to 5 wt% of SiO₂ nanofiller [30].

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Among the nanocomposite samples, the sample with 5 wt% of SiO₂ showed the highest resistance to electrical treeing. This shows that an appropriate loading of SiO₂ nanoparticles can effectively suppress the growth of an electrical tree. For the nanocomposite samples containing 6 wt% and 7 wt% of SiO₂, however, much shorter electrical tree breakdown times and much higher growth rates were recorded. This could be due to the agglomerated structure of SiO₂ nanoparticles within the nanocomposite samples. Severe nanofiller agglomerations, as depicted in Figures 7 (d) and 7 (e), could result in a much shorter path for a tree to propagate through the agglomerated SiO₂ surfaces.

5. Conclusion

In the investigated SiR/SiO₂ nanocomposites up to 5 wt% of SiO₂ loading levels, the electrical tree growth was slower compared with the unfilled SiR. The addition of SiO₂ nanofiller in SiR could, therefore, act as an inhibitor to retard the growth of electrical treeing. FTIR results showed that the SiO₂ nanofiller could have good physical interactions with the structure of the SiR. From the results of the electrical tree inception voltage, tree breakdown time, tree propagation length and tree growth rate, SiR/SiO₂ nanocomposites (up to 5 wt% of SiO₂ loading levels) showed advantageous electrical tree characteristics compared with the unfilled SiR.

From the current work, 5 wt% of SiO₂ loading was identified as the optimum amount for the SiR/SiO₂ nanocomposites. This nanocomposite formulation resulted in a desirable electrical tree resistance performance compared with other investigated samples. Therefore, it is generally envisaged that SiR/SiO₂ nanocomposites with 5 wt% of SiO₂ amount level can be utilized as electrical insulating materials for improving the discharge resistance performance and increasing the insulation lifetime of the silicone rubber insulating material.

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References

- Montanari GC, Mazzanti G, Simoni L. Progress in electrothermal life modeling of electrical insulation during the last decades. *IEEE Trans. Dielectr. Electr. Insul.* 2002; 9(5): 730–745.
- [2] Piah MAM, Darus A, Hassan A. Electrical tracking performance of LLDPE-natural rubber blends by employing combination of leakage current level and rate of carbon track propagation. *IEEE Trans. Dielectr. Electr. Insul.* 2005; 12(6): 1259–1265.
- [3] Baumann T, Fruth B, Stucki F, Zeller HR. Field-enhancing defects in polymeric insulators causing dielectric aging. *IEEE Trans. Electr. Insul.* 1989; 24(6): 1071–1076.
- [4] Kao KC. Dielectric Phenomena in Solids. Academic Press. 2004.
- [5] aughan AS, Dodd SJ, Sutton SJ. A Raman microprobe study of electrical treeing in polyethylene. *J. Mater. Sci.* Jan. 2004; 39(1): 181–191.
- [6] Vaughan AS, Hosier IL, Dodd SJ, Sutton SJ. On the structure and chemistry of electrical trees in polyethylene. *J. Phys. D. Appl. Phys.* 2006; 39(5): 962–978.
- [7] Dodd SJ, Champion JV, Zhao Y, Vaughan AS, Sutton SJ, Swingler SG. *Influence of morphology on electrical treeing in polyethylene blends*. IEE Proc. Sci. Meas. Technol. 2003; 150(2): 58–64.
- [8] Arief YZ, Ismail M, Makmud MZ, Adzis Z, Muhamad NA. Partial Discharge Characteristics of Natural Rubber Blends With Inorganic Nanofiller As Electrical Insulating Material. *Appl. Mech. Mater.* 2013; 284–287: 188–192.
- [9] Aulia, Abdul-Malek Z, Arief YZ, Piah MA, Jaafar M. Partial Discharge Characteristic of Low Density Polyethylene and Silica Nanocomposite. *Appl. Mech. Mater.* 2014; 554: 133–136.
- [10] Aulia, Ahmad MH, Abdul-Malek Z, Arief YZ, Lau KY, Novizon. Partial Discharge Characteristics in LLDPE-Natural Rubber Blends : Correlating Electrical Quantities with Surface Degradation. J. Electr. Eng. Technol. 2016; 11(3): 699-706.
- [11] Samuel JG, Lucas G, Fu M, Howard PJ, Lafon-Placette S. Nano-dielectrics research for application to high voltage insulation systems. 2012 47th International Universities Power Engineering Conference (UPEC). 2012: 1–6.
- [12] Singha S, Thomas MJ. Influence of filler loading on dielectric properties of epoxy-ZnO nanocomposites. *IEEE Trans. Dielectr. Electr. Insul.* 2009; 16(2): 531–542.

- [13] Frechette MF. Innovation in dielectric materials: from macro to nanoscales. Electrical Insulation Conference (EIC) 2009. 2009: 514–523.
- [14] Raetzke S, Kindersberger J. Role of interphase on the resistance to high-voltage arcing, on tracking and erosion of silicone/SiO2 nanocomposites. *IEEE Trans. Dielectr. Electr. Insul.* 2010; 17(2): 607–614.
- [15] Frechette MF, Reed CW. The role of molecular dielectrics in shaping the interface of polymer nanodielectrics. Annual Report-Conference on Electrical Insulation and Dielectric Phenomena, CEIDP. 2007; 2: 279–285.
- [16] Smith RC, Hui L, Nelson JK, Schadler LS. Interfacial charge behavior in nanodielectrics. 2009 IEEE Conference on Electrical Insulation and Dielectric Phenomena. 2009: 650–653.
- [17] Tuncer E, Sauers I. Industrial application perspectives of nanodielectrics. Dielectric Polymer Nanocomposites. 2010: 321–338.
- [18] Iizuka T, Ohki Y, Tanaka T. Effects of coupling agent and filler dispersion on Vt characteristics of epoxy/silica nanocomposites. Electrical Insulating Material (ISEIM 2008), IEEE International Symposium. 2008: 60-63.
- [19] Sridhar A, Thomas MJ. Electrical treeing in polyethylene: effect of nano fillers on tree inception and growth. High Voltage Engineering and Application (ICHVE). 2010 IEEE International Conference. 2010: 576-579.
- [20] Niedernhuber J, Kindersberger J. Electrical treeing in insulating resins with silica nanofillers. Solid Dielectrics (ICSD). 2013 IEEE International Conference. 2013: 828-831.
- [21] Du BX, Ma ZL, Gao Y, Han T, Xia YS. Effects of nano filler on treeing phenomena of silicone rubber nanocomposites. Electrical Insulation and Dielectric Phenomena (CEIDP), IEEE 2011 Annual Report Conference. 2011: 788-791.
- [22] Vlastos AE, Sherif E. Experience from insulators with RTV silicon rubber sheds and shed coatings. *IEEE Trans. Power Deliv*.1990; 5(4): 2030–2038.
- [23] Suwarno, Pratomosiwi F. Application of RTV silicone rubber coating for improving performances of ceramic outdoor insulator under polluted condition. Proceedings of the 2009 International Conference on Electrical Engineering and Informatics, ICEEI 2009. 2009; 2: 581–587.
- [24] Jung SY, Kim BK. Preparation and Characteristics of High Voltage Liquid Silicone Rubber by Modified Cross-linking Agent. *Trans. Electr. Electron. Mater.* 2009; 10(1): 9–15.
- [25] Ma YQ, Wu FL, Xu C. Nonlinear numerical analysis of high voltage cable terminal rubber stress cone. Mechanic Automation and Control Engineering (MACE), 2011 Second International Conference. 2011: 456-459.
- [26] Du BX, Gao Y. *Grow characteristics of electrical tree in silicone rubber*. Proceedings of the 16th International Symposium on High Voltage Engineering. 2009: 1–4.
- [27] Ahmad MH, Ahmad H, Bashir N, Arief YZ, Abdul-Malek Z, Kurnianto R, Yusof F. A New Statistical Approach for Analysis of Tree Inception Voltage of Silicone Rubber and Epoxy Resin under AC Ramp Voltage. Int. J. Electr. Eng. Informatics. 2012; 4(1): 27–39.
- [28] Gorur RS. Accelerated aging of silicone rubber cable terminations. Annual Report Conference on Electrical Insulation and Dielectric Phenomena. 1989: 155–160.
- [29] Bitinis N, Hernández M, Verdejo R, Kenny JM, Lopez-Manchado MA. Recent Advances in Clay/Polymer Nanocomposites. *Adv. Mater.* 2011; 23(44): 5229–5236.
- [30] Danikas MG, Tanaka T. Nanocomposites-a review of electrical treeing and breakdown. *IEEE Electr. Insul. Mag.* 2009; 25(4): 19–25.