# Characterization of Erbium Doped Photonic Crystal Fiber

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# Abstract

Photonic crystal fibers (PCFs) which exhibit unique and tremendous optical properties have been undergoing quick growth in recent years. Studies on the characteristics of various types of PCFs have been reported. However, characterization on erbium-doped PCF has not previously been investigated. Therefore, in this paper, an erbium-doped core PCF having 7 rings of hexagonal air holes has been modeled. A perfectly matched layer (PML) is modeled within the PCF structure and simulated using Finite Element Method (FEM) using COMSOL software. The PML is optimized by varying the radius and thickness of the layer. Modal properties of the PCF have been investigated in terms of its effective index of the supported fundamental mode, confinement loss and thickness of the perfectly matched layer. This erbium-doped PCF has a confinement loss of 1.0E-6 at 1500 nm and a maximum effective refractive index of 1.476. This paper gathers useful data, which could be used for studying the characteristics of a PCF.

**Keywords**: finite element method (FEM), erbium-doped photonic crystal fiber, COMSOL multiphysics, perfectly matched layer, confinement loss

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# 1. Introduction

A new class of waveguide, photonic crystal fibers (PCFs), has become an interesting and extensively developed subject in worldwide optical field research, leading to a large variety of designs and applications [1-6]. For example, PCF can be used in fiber sensors similar to those already presented; such as fiber Bragg gratings (FBG) in single mode fiber (SMF) for strain [7] and stress sensors utilizing multimode optical fiber (MMF) [8]. PCFs have unique and tremendous optical properties; such as endless single-mode operation, flexible design of airhole cladding, anomalous dispersion, high non-linearities, ultra-large-mode-area cladding and intrinsic polarization stability [9, 10]. A photonic crystal fiber which is also known as holey fiber is an optical fiber which gains its waveguide properties from very tiny and closely spaced air holes which are arrange throughout the whole length of the fiber. Such air holes can be obtained by using a preform with (larger) holes made. For example, by stacking capillary or solid tubes (stacked tube technique) and then inserting them into a larger tube [11, 12]. There exists an extensive variety of hole arrangements, thus leading to PCFs possessing very different properties.

PCFs are distinguished from standard "step-index" optical fibers by their cladding, formed by low refractive index inclusions; such as air holes that run along the entire fiber core length. PCFs have exceptional properties and features which are frequently better as compared to traditional fiber; such as lower bending losses, better chromatic dispersion compensation and endlessly single mode light propagation for a very broad wavelength range [13]. Furthermore, PCFs can be fabricated with specific properties by appropriate selecting the fiber microstructure, such as the hole size, distance between holes – lattice pitch, geometry and the air holes position.

Studies on the characteristics of various types of PCFs, in terms of chromatic dispersion, confinement loss, effective area and nonlinearity have been reported. For example, a solid core PCF has been modeled and the effective index, as well as the dispersion, have

been investigated via fundamental space-fill mode (FSM) layer [14]. Besides that, an index-guiding PCF has also been characterized via a new type of circular perfectly matched layer (PML) [15]. Additionally, characterization of a GeO<sub>2</sub>-doped PCF has been reported by inserting an extra GeO<sub>2</sub>-doped SiO<sub>2</sub> square in the core region, in order to control the waveguide properties of the fiber [9]. However, modeling on erbium-doped PCF has not previously been investigated.

Therefore, in this paper, a PCF containing an erbium-doped core, with seven rings of hexagonal air hole rings, is modeled. A finite element method, with a perfectly matched layer (PML), is used to compute the effective mode index and confinement loss. The PML is optimized by varying the radius and thickness of the layer. The RF physics feature of COMSOL MULTIPHYSICS is used in the simulation.

# 2. Design of PCF Structures

The cross-section of our model for hexagonal PCF has 7 rings of air holes, and is shown in Figure 1. The central core region is perturbed by erbium doping, and the background material used is silica. The diameter of air hole (d) and the pitch length ( $\Lambda$ ) (i.e. periodic length between the holes) are two PCF parameters which defines its geometrical structure. These parameters can be varied in order to control the properties of the PCF to a large extent. The parameters used in our modeling are shown in Table 1.

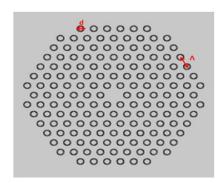


Figure 1. Geometry of Erbium Doped Photonic Crystal Fiber

Table 1. Simulation Parameters	
PARAMETER	VALUE (µm)
Cladding diameter	125
Hole diameter (d)	2.0
Pitch of holes $(\Lambda)$	4.0
Doped area	4.0
Mode field diameter	45

## 3. Theoretical Background

A Finite element method, with a perfectly matched layer (PML), was used for accurate modeling of the PCF. A circular, perfectly matched layer is created around the PCF structure. PML is an absorbing layer specially studied to absorb the incident radiation, without producing reflection of the electromagnetic waves. The PML can be defined by two parameters, which are the layer thickness (e) and internal radius ( $r_{in}$ ). The PML is schematically shown in Figure 2.

In the PML region, Maxwell's equation can be written as [15]:

$$\nabla \wedge \overset{\mathbf{P}}{\mathbf{H}} = j\omega \varepsilon_0 n^2 s. \overset{\mathbf{P}}{\mathbf{E}} \tag{1}$$

$$\nabla \wedge \vec{\mathbf{E}} = -j\omega\mu_0 s. \vec{\mathbf{H}} \tag{2}$$

882 ■ ISSN: 1693-6930

Where,

$$s = 1 - j. \frac{\sigma_e}{\omega \varepsilon_0 n^2} = 1 - j. \frac{\sigma_m}{\omega \mu_0}$$
(3)

Where E is the electric field, H is the magnetic field,  $\omega$  is the angular frequency,  $\varepsilon_0$  and  $\mu_0$  are the permittivity and permeability of vacuum respectively, n is the refractive index,  $\sigma_e$  and  $\sigma_m$  are the electric and magnetic conductivities of the PML respectively. Based on the m-power profile in Figure 2, a small reflection coefficient, R at the interface between the PML and the pure silica region shows that the absorption of the PML is optimal. To optimize R, electric conductivity can be written as:

$$\sigma_e = \sigma_{\text{max}} \left( \frac{\rho - r_{in}}{e} \right)^m \tag{4}$$

In this paper, the Erbium doped silica PCF is simulated based on the following theoretical conditions. The refractive index of silica in the simulation has been calculated using Sellmeier's equation [9] as given below:

$$n^2 = 1 + \sum_{i=1}^{3} \frac{A_i \lambda^2}{\lambda^2 - l_i} \tag{5}$$

Where  $A_i$  and  $I_i$  are the oscillator strength and oscillator wavelength respectively. The refractive index of erbium doped silica can be calculated from the following equation:

$$n^{2} = 1 + \sum_{i=1}^{3} \frac{(SA_{i} + X(EA_{i} - SA_{i}))\lambda^{2}}{\lambda^{2} - (SI_{i} + X(EI_{i} - SI_{i}))^{2}}$$
(6)

Where SA, SI, EA, EI are the Sellmeier coefficients for the silica and erbium respectively and X is the doping concentration of erbium. We had also calculated confinement loss which is defined by equation 7 [10]. Confinement loss is a fraction of leaky modes which is calculated from the imaginary part of the effective index of the fundamental mode, imag (neff).  $k_0$  is defined as the free space wave number and  $\lambda$  is the operating wavelength.

$$L_c = 8.686 k_0 imag(neff)[dB/m]$$
(7)

With:

$$k_0 = \frac{2\pi}{\lambda} \tag{8}$$

# 4. Modeling and Simulation

# 4.1. COMSOL Multiphysics

COMSOL Multiphysics is software that is based on finite element analysis used for modeling and solving variety of scientific and engineering problems. COMSOL consists of built-in physics interfaces, and has superior support for material properties by building the models based on the defined relevant physical quantities; such as material properties, loads, constraints, sources and fluxes. COMSOL Multiphysics then internally compiles a set of equations representing the entire model [16].

The software runs the finite element analysis, together with adaptive meshing and error control, using a variety of numerical solvers. In this paper, an RF Module is selected in order to solve problems in the general field of electromagnetic waves.

# 4.2. Modeling

Figure 3 shows the flowchart for the modeling of the PCF using COMSOL. It consists of 5 steps, and begins with geometry modeling based on the desired fiber structure. The next step is to specify the physical settings, followed by mesh generation. Next, it computes the solution for analysis purpose. Finally, the results are deduced using post processing and visualization tools.

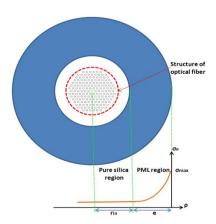


Figure 2. Schematic Diagram of PML

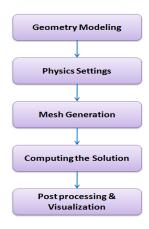


Figure 3. Flowchart for Modeling

In the geometry modeling step, an erbium-doped PCF, having 7 rings of hexagonal air holes, is designed via the COMSOL software, as shown in Figure 4. The PCF is designed and modeled, based on the structure of the scanning electron microscope (SEM) photograph (Figure 5). The SEM photograph is provided by Fiberhome Company. The geometrical structure of PCF is defined by few parameters; these are the diameter of air hole (d) which is  $2\mu m$ , pitch of holes ( $\Lambda$ ) which is  $4\mu m$ , doped area of  $4\mu m$  and cladding diameter of  $125\mu m$ .

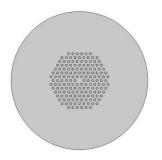


Figure 4. Simulated Profile

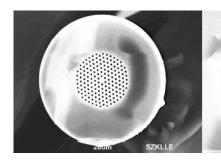


Figure 5. SEM Photograph

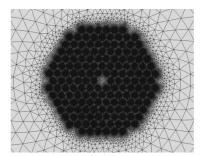


Figure 6. Mesh of the Structure



Figure 7. Solution Computed (The Red Portion Indicates the Highest Electric Field)

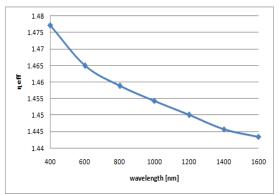
884 ■ ISSN: 1693-6930

The next step is to specify the physical settings; which include the material properties, wavelength of light, boundary condition and refractive index of the silica cladding, erbium core and the air holes via equation 5 and 6. This is followed by mesh generation, as shown in Figure 6

The characterization of the modeled structure is discreted into little units of simple form referred to as mesh elements. The physical properties and boundary conditions are expressed via each mesh element which is managed by a set of characteristic equations. These characteristics equations are explained as a set of simultaneous equations to calculate the effective index of the modes supported by the fiber [14]. The results are interpreted using post processing and visualization tools, as shown in Figure 7.

### 5. Results and Discussion

Figure 8 shows the variation of effective index of the fundamental mode. By using Comsol Multiphysics, effective refractive index of the fiber can be determined, which are useful for studying the characteristics of the PCF in terms of its chromatic dispersion, confinement loss, effective area and nonlinearity. The effective index result is in good agreement with previous work done [10, 14] - whereby the effective index decreases with wavelength. The maximum effective refractive index of this fiber is observed to be 1.476.

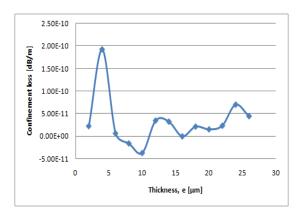


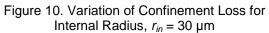
9.77E-11
1.95E-11
3.91E-12
7.81E-13
3.13E-14
6.25E-15
2.50E-16
5.00E-17
1.00E-17
3.0 35 40 45 50 55 60

r<sub>to</sub> [µm]

Figure 8. Effective Index of the Fundamental Mode

Figure 9. Variation of Confinement Loss in 26 µm Radius Structure





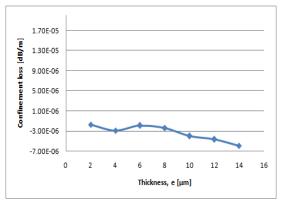


Figure 11. Variation of Confinement Loss for Internal Radius,  $r_{in} = 50 \mu m$ 

Figure 9 shows the optimization of the perfectly match layer (PML) by varying the layer thickness (e) along the internal radius ( $r_{in}$ ) at 1550 nm. Based on the principal of PML, the layer

should be placed far from the structure of the fiber. It should be large enough to obtain less variation of confinement loss. In the in-set of Figure 9, the structure of the PML is shown. For a thickness of 2  $\mu$ m, the variation of confinement loss is large, compared to thicknesses of 6  $\mu$ m and 10  $\mu$ m. The thickness of 10  $\mu$ m is adequate to obtain less variation of confinement loss.

Figure 10 and Figure 11 show the variation of confinement for internal radius,  $r_{in}$  of 30  $\mu$ m and 50  $\mu$ m, respectively, at 1550 nm. For an internal radius of 30  $\mu$ m, a thickness of more than 12  $\mu$ m is sufficient to obtain less variation of confinement loss. On the other hand, an internal radius of 50  $\mu$ m shows less variation of confinement loss along the whole range of thickness. In this case, the thickness of the PML is not a curial parameter, as the internal radius is large enough to evaluate less variation of confinement loss.

The calculation of confinement loss as a function of wavelength for internal radius,  $r_{in} = 50 \mu m$  and PML thickness,  $e = 12.5 \mu m$ , is shown in Figure 12. The confinement loss shows an almost linear relationship with wavelength. This erbium doped photonic crystal fiber has a confinement loss of  $1.0E^{-6}$  at 1500 nm. This result is in good agreement with previous work done [9, 10] whereby the confinement loss increases with wavelength.

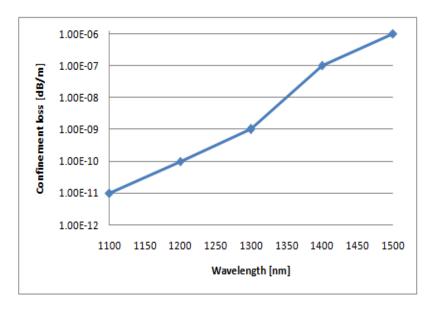


Figure 12. Confinement Loss for Internal Radius,  $r_{in}$  Of 50 µm and Thickness, E Of 12.5 µm

# 6. Conclusion

We have modelled and simulated an Erbium doped PCF core, with 7 rings of hexagonal air holes, using COMSOL Multiphysics. The Finite element method, with a perfectly matched layer (PML), has been used for accurate modeling of the PCF. The geometrical structure and numerical results of the effective index and confinement loss of the fiber have been presented. The PML layer, which is placed far from the structure of the fiber, shows less variation of confinement loss. Internal radius and thickness layer are two crucial parameters needed for optimization of the PML. This paper gathers useful data, which could be used for studying the characteristics of a PCF.

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886 ■ ISSN: 1693-6930

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