

Phase Open Fault Tolerant Control of High Reliability Doubly-Salient Wound-Field Machine

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Abstract

Doubly Salient Wound-Field Machine (DSWFM) can be employed on aeronautics starter-generator because it has good performance on both power generation and starting. To improve the system reliability, a three-phase four bridge legs converter which has fault tolerant capability is proposed to solve one phase open-circuit fault problem of the DSWFM. And the advantage of the proposed converter to the full-bridge converter fault-tolerant mode is analyzed. With the study of DSWFM theory and torque equation, a constant torque fault-tolerant strategy is proposed to keep the performance and reduce the torque ripple. The drive system after fault identification can be reconstructed by the proposed method, and the machine performance can recover quickly. Simulations confirm the feasibility of the proposed fault tolerant system.

Keywords: Doubly Salient Electro-magnet Machine (DSWFM); Fault Tolerant; Converter; Phase Open

1. Introduction

Doubly Salient Wound-Field Machine (DSWFM) is a new type of brushless DC machine that comes from DSPM by using field winding instead of permanent magnet excitation in 1990s[1]-[3]. Its armature windings and excitation windings are both mounted on the SRM-structured stator, and it is with similar salient rotor structure to SRM rotor. DSWFM has such advantages as simple structure, low cost, high reliability and good fault-tolerance [4]-[6]. Thus it has good application prospects in many fields including wind power generation, aeronautics, astronautics, automobiles and ships, especially in engine starter-generator.

The reliability of the DSWFM system is extremely important in starter-generator, fuel transmission and braking application. To improve the reliability of the whole system, several papers have studied about the development for fault tolerant inverter system, because the inverter is the weakest link of the motor drive system[7]-[12]. But these papers just focus on traditional machine such as PM machine and induction machine. As DSWFM machine is deferent from those traditional machine, it is necessary to develop a new fault-tolerant topology and a new control strategy to improve the reliability of the DSWFM system.

Based on the analysis of special characteristics of DSWFM system, this paper proposes a simple fault detection and isolation scheme when a open-switch fault occur in the full-bridge inverter of DSWFM. After fault identification, faulty leg will be isolated by control signal. The system after faults is operated with fault tolerant mode. The theoretical operating principle of DSWFM and the proposed fault detection identification algorithm are explained in detail. Simulation results verify the proposed fault tolerant scheme.

2.Principle and Analysis

The typical structure of DSWFM is shown in Figure 1: It has 12 stator poles, 8 rotor poles and four excitation winding coils. Each stator has a concentrated phase windings independently, and the phase winding coils with the same electric angle is linked in series, which build Phase A, B and C.

In the double-beat working mode, a full-bridge inverter is the best inverter topology used for DSWFM, it is shown in Figure 2.

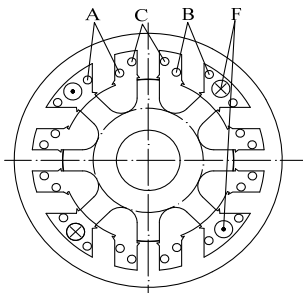


Figure 1 Cross section of DSWFM

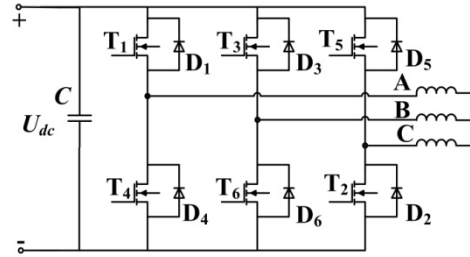


Figure 2. Full-bridge converter topology on DSWFM

Without the consideration of such factors as side effect, magnetic reluctance of core, and so on, the phase self-inductance L_p and mutual-inductance between phase and exciting winding L_{pf} of each phase makes the distribution in Figure 3. And its values have relationship with rotor angle but not with stator current. While the phase current i_p is shown in Figure 3.

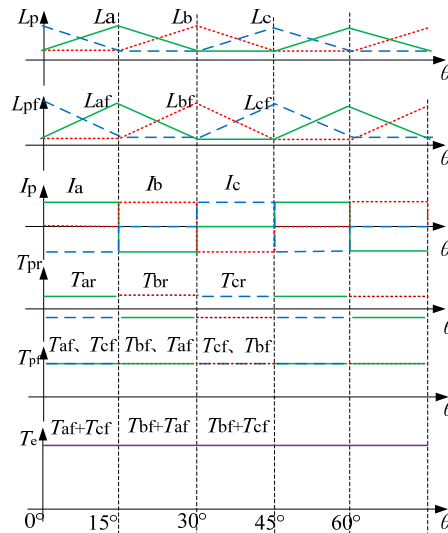


Figure 3. Output torque of a normal DSWFM

One phase torque equation of DSWFM is shown in [14]

$$T_p = \frac{1}{2} i_p^2 \frac{dL_p}{d\theta} + i_p i_{if} \frac{dL_{pf}}{d\theta} \tag{1}$$

$$= T_{pr} + T_{pf}$$

Where T_p is the output torque of phase p, T_{pr} is the phase magnetic resistance torque, T_{pf} is the phase excitation torque, i_p is the excitation current, L_p is the phase self-inductance, L_{pf} is the mutual-inductance, θ is the rotor position angle. For a 12/8 poles DSWFM, the output torque of a normal DSWFM can be drawn in Figure 1. Generally, T_{pr} is much smaller than T_{pf} in their absolute values.

T_{pr} produced by two phase windings can cancel out each other [14]. When switch T1, T4 are turned on, phase A and C works, in other words, the machine works in $[0^\circ, 15^\circ]$ sector in Figure1, for example:

$$i_a = -i_c = i$$

The positive current in phase A produces positive torque due to the increasing flux, the negative current of phase C also produce positive torque due to the dropping flux. So the output torque of phase A and C is:

$$\begin{cases} T_a = \frac{1}{2} i_a^2 \frac{dL_a}{d\theta} + i_a i_f \frac{dL_{af}}{d\theta} \\ T_c = \frac{1}{2} i_c^2 \frac{dL_c}{d\theta} + i_c i_f \frac{dL_{cf}}{d\theta} \end{cases} \quad (2)$$

Because of $\frac{dL_a}{d\theta} = -\frac{dL_c}{d\theta}$, $\frac{1}{2} i_a^2 \frac{dL_a}{d\theta} = -\frac{1}{2} i_c^2 \frac{dL_c}{d\theta}$, Let

$$\frac{dL_{af}}{d\theta} = -\frac{dL_{cf}}{d\theta} = k_L \quad (3)$$

So the total output torque of the machine is :

$$T_e = T_a + T_c = i_a i_f \frac{dL_{af}}{d\theta} + i_c i_f \frac{dL_{cf}}{d\theta} = 2T_{pf} = 2i_i k_L \quad (4)$$

3. Fault Tolerant Mechanism of DSWFM

3.1 Fault Detection and Identification

Because of the T1, T2 open fault has the same performance with phase A open winding, both of the phase windings and inverter failure can be classified as phase open fault. Moisture, overheat, erosion environment and the impact of external forces can cause damage to the DSWFM winding, these fault can also be divided into open-circuit fault and short-circuit fault. The inverter is the weakest link of the system, it can be suffered by the open-circuit fault and short-circuit fault. The open-circuit fault occurs due to over-current or control device deterioration, the short-circuit fault also often happens because of over-voltage.

The phase short faults are often protected by fuse. So this paper mainly introduced phase open faults.

For example, in Figure 2, when phase C is open, it should be removed immediately. Then phase A and B can not form a circuit loop with phase C. As shown in Figure 3, in $[15^\circ, 30^\circ]$, the output torque of the motor is normal. But the motor output torque is 0 in $[0^\circ, 15^\circ]$ and $[30^\circ, 45^\circ]$, as shown in Figure 3. So it is necessary to reconstruct the system converter to achieve fault-tolerant operation.

Phase open fault detection can be realized by three-phase current sensor. Because the three-phase winding conducts pairwise, when the rotor is in $[0^\circ, 15^\circ]$, phase A and C current is normal, while in the other period this two phases current are greater than 1.5 times or less than 0.2 times the predetermined current, then short-circuit or open-circuit fault of phase B can be drawn from this phenomenon. In this way, we can determine the short-circuit or open-circuit fault of the other phases.

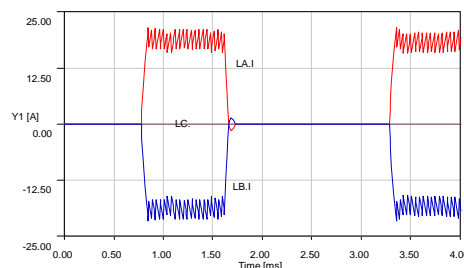


Figure 3. Three phase current when phase C is open

Phase winding with short-circuit or open-circuit fault should be disconnected by the fuse and control system, and the machine should be operated on fault-tolerant mode.

3.2 Full-bridge Converter Fault-tolerant Mode

For the same example, when phase C is on open-circuit fault, it will not conduct in $[0^\circ, 15^\circ]$. We can turn on T1 and T6 to power phase A and phase B to drive the motor in fault-tolerant mode in $[0^\circ, 15^\circ]$. In $[15^\circ, 45^\circ]$, we can turn on T3 and T4 to supply power to phase B and phase A. Three phase current of DSWFM on full-bridge converter fault-tolerant mode is shown in Figure 4. And DSWFM output torque on phase C open full-bridge converter fault-tolerant mode is shown in Figure 5.

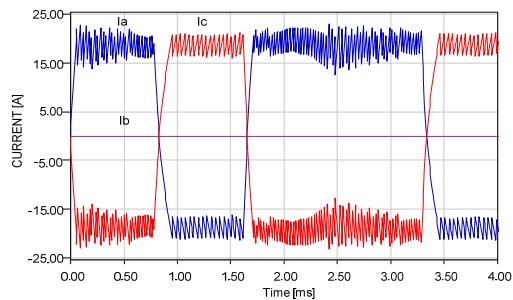


Figure 4. Three phase current on phase C open full-bridge converter fault-tolerant mode

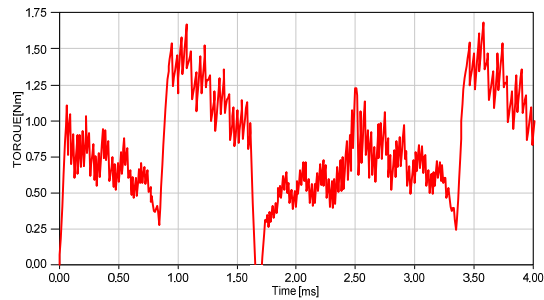


Figure 5. DSWFM output torque on phase C open full-bridge converter fault-tolerant mode

However, this fault-tolerant mode has three shortcomings:

First of all, phase B and A energized at the same time but only one phase can generate torque, the other phase plays the role of a loop winding, which reduces the efficiency of the motor; At the same time, phase B and A work at the full time and its large current may cause a system failure; In addition, the phase B and A pass the same circuit, their excitation torque is equal, but its reluctance torque is in the opposite direction, it will generate a lot of torque ripple.

3.3 Three-phase Four Bridge Legs Converter Fault-tolerant Mode

Owing to the connection of two-phase, of DSWFM machine with full-bridge converter has low performance in fault tolerant operation. To meet the requirement of the electric independence, a fault tolerant motor drive should detect and isolate the fault phase without any effect on other healthy phases. The machine can be operated with other healthy phases working during loss of one phase.

A high reliability, three-phase four bridge legs converter which has fault tolerant capability is proposed in Figure 6 to solve one phase open-circuit fault problem of the DSWFM. It only applies two more switches than the traditional full-bridge converter, and it can avoid the above shortcomings of the full bridge converter fault-tolerant mode.

For the same example, when phase C is on open-circuit fault, we can turn on T1 and T8 to power phase A to drive the motor in fault-tolerant mode in $[0^\circ, 15^\circ]$, as shown in Figure 7, the total output torque is the sum of phase A magnetic resistance torque T_{ar} and phase A excitation torque T_{af} . As self-inductance of phase A and mutual-inductance between phase A and exciting winding F is in the increase, T_{ar} and T_{af} both large than 0.

In $[15^\circ, 30^\circ]$, the output torque of the motor is normal.

In $[30^\circ, 45^\circ]$, we can turn on T7 and T6 to power phase B to drive the motor in fault-tolerant mode. The total output torque is the sum of phase B magnetic resistance torque T_{br} and phase B excitation torque T_{bf} . As self-inductance of phase B and mutual-inductance between phase B and exciting winding L_{bf} is in the decrease, $T_{af} > 0$ and $T_{ar} < 0$.

The full-bridge converter fault-tolerant mode and three-phase four bridge legs converter tolerant mode is compared in Table 1. The four bridge legs converter tolerant mode has no loop

winding, this increases the efficiency of the motor. In addition, the four bridge legs converter tolerant mode windings current of the two phase can be controlled individually to achieve a smooth output torque.

Table 1 .Comparison between Full-bridge and Three-phase Four Bridge Legs Converter Fault-tolerant Mode

	[0°, 15°]	[15°, 30°]	[30°, 45°]
Normal working switch	T1,T2	T3,T4	T5,T6
Normal working winding	A,-C	B,-A	C,-B
Full-bridge converter fault-tolerant mode working switch	T1,T6	T3,T4	T1,T6
Full-bridge converter fault-tolerant mode working winding	A,-B	B,-A	A,-B
Four bridge legs converter fault-tolerant mode working switch	T1,T8	T3,T4	T7,T6
Four bridge legs converter fault-tolerant mode working winding	A	B,-A	-B

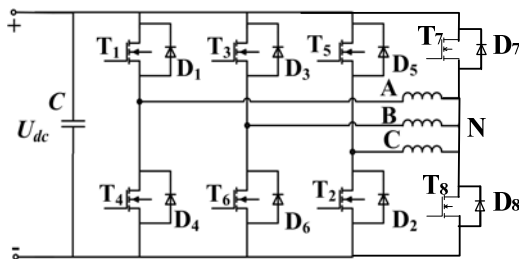


Figure 6 Three-phase four bridge legs fault-tolerant converter

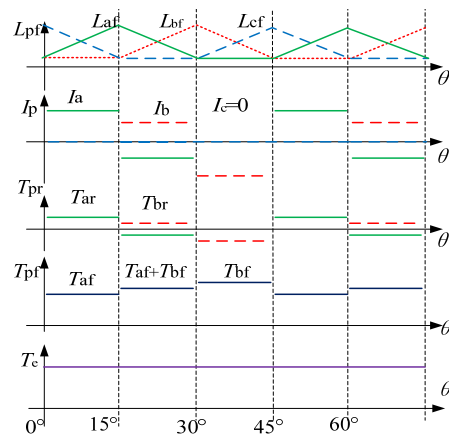


Figure 7 Three-phase four bridge legs converter fault-tolerant mode

4. Constant Torque Fault-tolerant Strategy

Assuming the normal output torque of the motor:

$$T_e = 2T_{pf} = 2i_f k_L$$

With the proposed four bridge legs converter fault-tolerant mode, if the current of phase A and B is equal to the normal state when phase C is on open-circuit fault, then the output torque of the motor T'_e :

$$T'_e = \begin{cases} T'_{e1} = i_a i_f \frac{dL_{af}}{d\theta} + i_c i_f \frac{dL_{cf}}{d\theta}; & [0^\circ, 15^\circ] \\ T'_{e2} = i_a i_f \frac{dL_{af}}{d\theta} + \frac{1}{2} i_a^2 \frac{dL_a}{d\theta}; & [15^\circ, 30^\circ] \\ T'_{e3} = i_c i_f \frac{dL_{cf}}{d\theta} + \frac{1}{2} i_c^2 \frac{dL_c}{d\theta}; & [30^\circ, 45^\circ] \end{cases} \quad (5)$$

In order to reduce the torque ripple, the winding number of the exciting winding is designed much larger than the armature winding. So the DSWFM excitation torque is larger than the reluctance torque and play a major role. Therefore, the output torque of the motor in [15°, 45°] is approximately equal to half of the normal output torque.

We can keep the output torque in fault-tolerant state of the same by changing three-phase current.

Assuming the current of phase A in [15°, 30°] is i_{a2} , and the current of phase C in [30°, 45°] is i_{c3} , then the output torque: T_e'' :

$$T_e'' = \begin{cases} T_{e1}'' = i_a i_f \frac{dL_{af}}{d\theta} + i_c i_f \frac{dL_{cf}}{d\theta}; & [0^\circ, 15^\circ] \\ T_{e2}'' = i_{a2} i_f \frac{dL_{af}}{d\theta} + \frac{1}{2} i_{a2}^2 \frac{dL_a}{d\theta}; & [15^\circ, 30^\circ] \\ T_{e3}'' = i_{c3} i_f \frac{dL_{cf}}{d\theta} + \frac{1}{2} i_{c3}^2 \frac{dL_c}{d\theta}; & [30^\circ, 45^\circ] \end{cases} \quad (6)$$

That is to say, we can keep the three-phase armature current of the motor be consistent with the equation (6) in order to ensure the output torque constant.

5. Simulation and Verification

A prototype machine of DSWFM has been designed. Table 2 gives key parameters of the machine.

Table 2. Protatype machine parameters

Items	Value
Number of stator poles	12
Number of rotor poles	8
Stator outer diameter	173mm
Stator inner diameter	112mm
Length of air-gap	0.35mm
Number of armature turns per pole	5
Number of turns per field coil	110
Width of a rotor pole	14.4mm
Stack Length	60mm

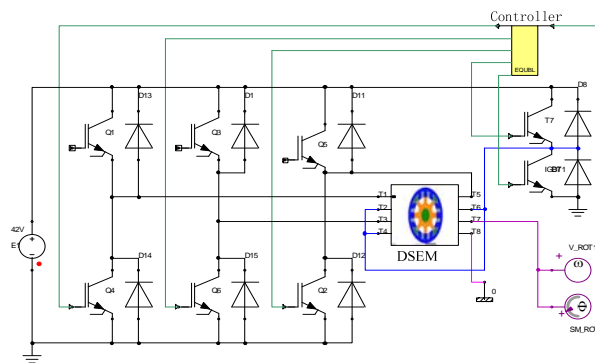


Figure 8 Simulation Model of DSWFM Phase Open Fault Tolerant

In equation (6), let $T_{e1}'' = T_{e2}'' = T_{e3}''$, then three-phase current of the prototype machine in Table II with C winding open can be obtained with the finite element method. They should be consistent with:

$$\begin{cases} i_a'' = \begin{cases} i_a; & [0^\circ, 15^\circ] \\ -2.4i_a; & [15^\circ, 30^\circ] \\ 0; & [30^\circ, 45^\circ] \end{cases} \\ i_b'' = 0; & [0^\circ, 45^\circ] \\ i_c'' = \begin{cases} -i_a; & [0^\circ, 15^\circ] \\ 0; & [15^\circ, 30^\circ] \\ 1.6i_a; & [30^\circ, 45^\circ] \end{cases} \end{cases} \quad (7)$$

In order to assess the aforementioned normal and faulty-tolerant performance of the DSWFM machine, the cosimulation technique is adopted in which the magnetic circuit and the electric circuit are coupled in the time domain. The modeling tools for the cosimulation are composed of three packages, the 2D FEA model, three-phase four bridge legs fault-tolerant converter model and controller model. The magnetic solver performs with coupled field-circuit is established and shown in Figure 8.

At each cosimulation time step, both the magnetic and circuit solvers exchange the calculated data, and the results produced by one solver will be exported to another solver in the next step. Consequently, the system performances can be accurately simulated.

Three phase current of DSWFM on under constant torque fault-tolerant strategy is shown in Figure 9. And DSWFM output torque is shown in Figure 10.

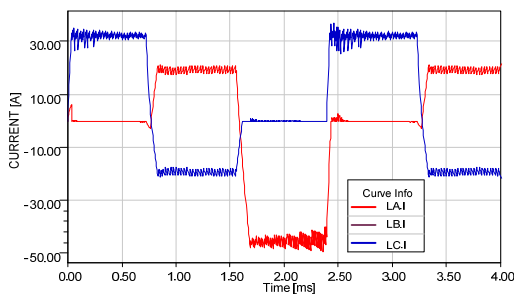


Figure 9 Three phase current under constant torque fault-tolerant strategy

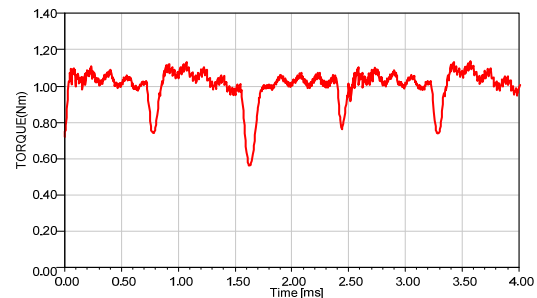


Figure 10 Output torque under constant torque fault-tolerant strategy

The state in [0ms, 0.8ms] is corresponding to motor mechanical angle in $[0^\circ, 15^\circ]$ in equation (7), the current of phase A is 1.6 times of the rated current. The state in [0.8ms, 1.6ms] is corresponding to motor mechanical angle in $[15^\circ, 30^\circ]$, its phase current is equal to the normal mode. The state in [1.6ms, 2.4] is corresponding to motor mechanical angle in $[30^\circ, 45^\circ]$. At this time, the current of phase C is -2.4 times of the rated current. The output torque under constant torque fault-tolerant strategy is almost equal to the normal working time.

6. Conclusion

The DSWFM system can be reconstructed after fault identification by the proposed four bridge legs converter tolerant mode, and the machine performance can recover quickly.

The proposed four bridge legs converter tolerant mode has no loop winding, which increases the efficiency of the motor. In addition, the four bridge legs converter tolerant mode windings current of the two phase can be controlled individually to achieve a smooth output torque.

With the constant torque fault-tolerant strategy, the proposed system can keep the normal performance with phase open fault and reduce the torque ripple. Simulations confirm the feasibility of the proposed fault tolerant system.

This paper laid the foundation for the rest of next experiments.

Acknowledgment

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